# **Semiconductor Physics**

#### Chapter 5, Bipolar transistors

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Symbols and nomenclature: npn- and pnp-transistors





**Biasing configurations** 



Common-Base



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#### **Biasing configurations**



#### Common-Emitter



#### **Biasing configurations**



Common-Collector



Connection and biases in common-base configuration



**Doping profiles and critical dimensions** 





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Energy band diagram of a npn transistor





#### **Electron currents**

#### Emitter and collector edge

$$0 = -\frac{n_p - n_{po}}{\tau_n} + D_n \frac{d^2 n_p}{dx^2}$$
$$n_p(x) = n_{po} + C_1 exp\left(\frac{x}{L_n}\right) + C_2 exp\left(\frac{-x}{L_n}\right)$$

 $C_1$  and  $C_2$  are constants and  $L_{\equiv}\sqrt{D_n\tau_n}$ 

$$C_{1} = \left\{ n_{p}(W) - n_{po} - \left[ n_{p}(0) - n_{po} \right] exp\left(\frac{-W}{L_{n}}\right) \right\} / 2 \sinh \frac{W}{L_{n}}$$

$$C_{2} = \left\{ \left[ n_{p}0 - n_{po} \right] exp\left(\frac{W}{L_{n}}\right) \left[ n_{p}(W) - n_{po} \right] \right\} / 2 \sinh \frac{W}{L_{n}}$$



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#### **Electron currents**

Emitter and collector edge

Boundary conditions for the two edges of the base:

$$n_{p}(0) = n_{po}exp\left(\frac{qV_{BE}}{kT}\right)$$

$$n_{p}(W) = n_{po}exp\left(\frac{qV_{BC}}{kT}\right)$$

$$I_{nE} = \frac{A_{E}qD_{n}n_{po}}{L_{n}}coth\frac{W}{L_{n}}exp\left(\frac{qV_{BE}}{kT}\right)$$

$$I_{nC} = \frac{A_{E}qD_{n}n_{po}}{L_{n}}cosech\frac{W}{L_{n}}exp\left(\frac{qV_{BE}}{kT}\right)$$

The ratio of  $I_{nC}/I_{nE}$  is called **base transport factor**  $\alpha_T$ 

#### **Electron currents**

Emitter and collector edge

$$I_{nE} \approx I_{nC} \approx \frac{A_E q D_n n_{po}}{W} exp\left(\frac{q V_{BE}}{kT}\right) \approx \frac{A_E q D_n n_i^2}{W N_B} exp\left(\frac{q V_{BE}}{kT}\right)$$

Can be reduced to:

$$I_{nE} \approx I_{nC} \approx \frac{2A_E D_N Q_B}{W^2}$$

 $Q_B$  is the injected excess charge in the base:

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$$Q_B = q \int_0^W [n_p(x) - n_{po}] dx$$



# **Doping profile**



#### **Electron Currents**

A build-in electric field enhances electron transport.

$$p(x) \approx N_B(x) = n_i exp\left(\frac{E_i - E_F}{kT}\right)$$

built-in field

$$\mathscr{E}(x) = \frac{dE_i}{qdx} = \frac{kT}{qN_B}\frac{dN_B}{dx}$$



#### **Electron Currents**

$$I_n(x) = A_E q \left( \mu_n \mu_p \mathscr{E} + D_n \frac{dn_p}{dx} \right)$$

substituting  $\mathscr{E}$ 

$$I_n(x) = A_E q D_n \left( \frac{n_p}{N_B} \frac{dN_B}{dx} + \frac{dn_p}{dx} \right)$$

steady state solution with boundary condition  $n_p(W) = 0$ 

$$n_p(x) = \frac{I_n(x)}{A_E q D_n N_B(x)} \int_x^W N_B(x) dx$$



#### **Electron Currents**

total impurity dose per area in the base

$$N_b \equiv \int_x^W N_B(x) dx$$

called Gummel number. (Si:  $10^{12} to 10^{13} cm^{-2}$ )



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#### **Hole Currents**

diffusion current injected from base to emitter

$$I_{pE} = \frac{A_E q D_p E p_{noE}}{W_E} \left[ exp\left(\frac{q V_{BE}}{kT}\right) - 1 \right]$$



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### **Recombination**

- Shockley-Read-Hall recombination
- Auger recombination

$$\frac{1}{\tau} = \frac{1}{\tau_n} + \frac{1}{\tau_A}$$

Base-emitter recombination

$$I_{rE} \propto rac{1}{ au} exp\left(rac{qV_{BE}}{mkT}
ight)$$



### **Collector base junction**

$$I_{CO} \approx A_C q \left( \frac{D_{pC} p_{noC}}{W_C - W_{DC}} + \frac{D_n n_{po}}{W} \right)$$



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### **Current gain**

$$I_E = I_{nE} + I_{rE} + I_{pE}$$

$$I_C = I_{nC} + I_{CO}$$

$$I_B = I_{pE} + I_{rE} + (I_{nE} - I_{nC}) - I_{CO}$$

It holds true that

 $I_E = I_C + I_B$ 







#### Parameters for a Bipolar Transistor



Common base current gain

 $I_{CBO}$ 

$$\alpha_0 \equiv h_{FB} = \frac{I_C - I_{CB0}}{I_E} = \frac{I_{nC}}{I_E} = \frac{I_{nC}}{I_n E} \frac{I_{nE}}{I_E} = \alpha_T \gamma$$

 $\gamma$  is defined as emitter injection efficiency



**Common emitter configuration** 

$$I_{\rm C} = \beta_0 I_B + I_{\rm CEO}$$

 $I_{CEO}$  is  $I_{CO}$  when  $I_B = 0$ , or open base:

$$I_C = \alpha_0 (I_B + I_{CO}) + I_{CBO}$$
$$= \frac{\alpha_0}{1 - \alpha_0} I_B + \frac{I_{CBO}}{1 - \alpha_0}$$
$$\Rightarrow \beta_0 \equiv h_{FE} = \frac{\alpha_0}{1 - \alpha_0}$$



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Base transport factor, emitter injection efficiency

Base transport factor

$$\alpha_T \equiv \frac{I_{nC}}{I_{nE}} = \frac{1}{\cosh(W/L_n)} \approx 1 - \frac{W}{2L_n^2}$$

Emitter injection efficiency

$$\gamma \equiv \frac{I_{nE}}{I_E} \approx \frac{I_{nE}}{I_{nE} + I_{pE}} \approx \left[1 + \frac{p_{noE}D_{pE}L_n}{N_{PO}D_nW_E} \tanh\left(\frac{W}{L_n}\right)\right]^{-1}$$



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$$h_{FE} = rac{\gamma}{1-\gamma} = rac{n_{po}D_nW_E}{p_{noE}D_{pE}L_n} \operatorname{coth}\left(rac{W}{L_n}
ight) \propto rac{n_{po}}{p_{noE}W} \propto rac{N_E}{N_BW} \propto rac{N_E}{N_b'}$$



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### **Output Characteristics**

- **①** applied voltages control the boundary densities through the term exp(qv/kT)
- emitter and collector currents are given by minority density gradients at x=0 and x=W (junction boundaries)
- Base current is the difference between emitter and collector current



Emitter bandgap narrowing

To improve  $h_{FE}$ , the emitter should be much more heavily doped than the base, that is  $N_E >> N_B$ . At high doping concentrations bandgap narrowing has to be considered. Bandgap reduction:

$$\Delta E_g = 18.7 \ln \left(\frac{N}{7 \cdot 10^{17}}\right)$$

N larger than  $7\cdot 10^{17}$  Intrinsic carrier density in the emitter is:

$$n_{iE}^2 = N_C N_V \exp\left(-\frac{E_g - \Delta E_g}{kT}\right) = n_i^2 \exp\left(\frac{\Delta E_g}{kT}\right)$$

 $n_i$ : intrinsic carrier density

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Emitter bandgap narrowing

Minority carrier concentration becomes

$$p_{noE} = \frac{n_{iE}^2}{N_E} = \frac{n_i^2}{N_E} \exp\left(\frac{\Delta E_g}{kT}\right)$$

Increased minority carrier concentration in the emitter. The net result is an increased hole diffusion current and the current gain is recuded

$$h_{FE} \propto rac{n_{po}}{p_{noE}} \propto \exp\left(-rac{\Delta E_g}{kT}
ight)$$



Kirk Effect

In modern bipolar transistors with a lightly doped collector region, the net charge is changed significantly under high-current condition. The high-field region is relocated from the base-collector junction towards the n+-substrate.

It is referred to as the Kirk effect and increases the effective Gummel number and causes a reduction of  $h_{FE}$  (current gain).



**Current Crowding** 

Minimization of the emitter resistance results in non-uniform current passing through the emitter area.



 $S_{ef}$  effective width carries most of the current.





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